

Kinetic and thermodynamic aspects of flotation beneficiation of polymetallic raw materials

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Abstract: The article presents the results of the development of a methodological approach to the analysis of kinetic and thermodynamic parameters for improving the efficiency of flotation processing of polymetallic raw materials. The kinetic dependences of flotation, the hydrophobizing ability of butyl potassium xanthogenate, and the effect of reagents on preliminary mechanical activation were studied, and flotation modeling with and without an oxidizer was performed. The best results of convergence with the kinetic dependences of flotation are shown by the Beloglazov equation, the Kelsall and the modified Kelsall models. Technological indicators of sulfide flotation in the presence of oxidants are higher, which can be explained by the intensive oxidation of the formed transient ions on the surface of minerals, which contributes to the alignment of the flotation properties of the surface. It is possible to integrate the proposed research methods into technological schemes in order to optimize technological indicators and increase profits.

1 Introduction

Over time, the quality of processed ores and the content of metals in them continuously decrease. Over the past 20 years, the content of non-ferrous metals in ores has decreased by 1.3-1.5 times, the share of hard-to-enrich ores has increased to 40 % of the total mass of raw materials received for processing.

Increasingly stringent requirements for the complex use of raw materials on the background of depletion of known balance deposits of non-ferrous and noble metals requires the use of new approaches in the enrichment of these raw materials [1].

To optimize technological indicators and increase the economic efficiency of processing polymetallic ores, it is necessary to use the kinetic and thermodynamic dependencies of flotation ore enrichment at the stage of designing technological schemes.

Kinetic studies and the distribution of minerals by floatability are necessary both for assessing ore enrichment at the initial stage and at the stage of a more detailed study. The study of flotation kinetics can be used to determine the time required for flotation.

The presence of an oxidized film on the surface of minerals changes their wettability characteristics, which affects the technical indicators of the flotation process. Effects occurring on the surface of minerals during oxidation can be used for selective extraction of each sulfide and selection of the reagent mode for both grinding and flotation [2].

Due to the oxidation of xanthogenate to insoluble dixanthogenide in the process of sulfide flotation, the sorption form on the surface of the mineral may change.

The purpose of this study is the development of a methodological approach to analyzing kinetic and thermodynamic parameters for improving the efficiency of flotation processing of polymetallic raw materials. To achieve this goal, the following tasks were set:

- Determine the zone of optimal values of the redox potential of the pulp for selective separation of minerals by thermodynamic modeling;
- Perform experimental studies to find the kinetic dependencies of the flotation process;
- Determine the dependence of the extraction of various minerals depending on the oxidizer;
- Compare the extraction values for flotation in the presence and absence of an oxidizer.

The kinetics of the flotation process is characterized by the dependence of mineral extraction on time. Based on the results of flotation kinetics analysis, it is possible, for example, to justify the optimal distribution of foam removal along the flotation front, compare and evaluate the floatability of different minerals in different conditions, identify the effect of certain flotation factors. It is necessary to distinguish the kinetics of flotation from the kinetics of a chemical reaction. The chemical reaction constant evaluates the probability of conversion, while the constant of flotation kinetics determines, generally speaking, the process of fixing and removal of mineral particles.

All kinetic models can be divided into fundamental, i.e. based on the physical and chemical aspects of the flotation act, and empirical, obtained for specific data by regression processing [3]

In practice, the first-order kinetic equation (the model of K. F. Beloglazov) is mostly used [4]. Many researchers have proposed more precise models to describe the flotation kinetics of various minerals (Fig. 1).

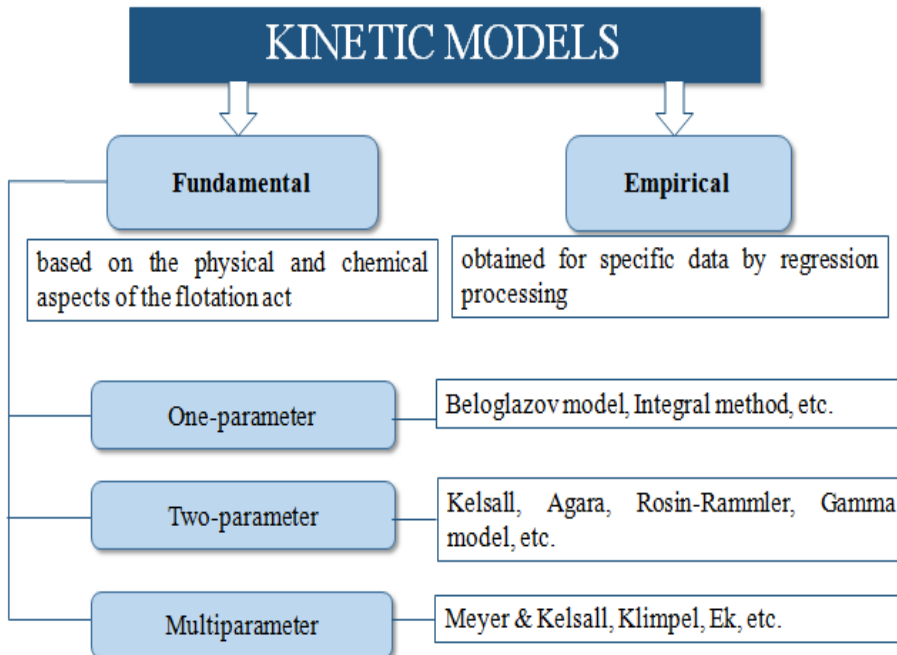


Fig. 1. Kinetic models of flotation beneficiation.

The selection of the Eh and pH range is necessary for selective flotation of minerals while keeping the stability of their oxidation process. Under these conditions, it is possible to select optimal concentrations of oxidants to improve the required technological indicators. The zone of stable existence of sulfate ions will be the optimal flotation zone of the raw material [5].

2 Materials and methods

Carbon-containing sulfide copper-zinc and gold-containing ores were selected as the objects of research.

Dictionem shales are grayish-black, black, and brown thinly layered carbonaceous rocks. This is low-grade oil shale due to its high ash content.

The choice of shale as an object of research is due to the importance of this object as a source of strategic metals, such as precious, rare, non-ferrous metals, and trace elements [6,7,8].

Copper-pyrite ores are an important industrial type of copper-sulfide ores. The main valuable components are copper, zinc, and sulfur. The development of these deposits is profitable due to the possibility of complex processing of raw materials, that is, the accompanying extraction of components with copper (zinc, gold, silver, sulfur, iron), the cost of which is significantly higher than the cost of copper [9].

For sulfide gold-containing ores, resistance is a characteristic feature. As a rule, gold-containing sulfides (mainly pyrite and arsenopyrite) have a crystal structure that is poorly permeable to cyanide solutions. Most of the grains of native gold in them have thin and ultra-thin dimensions. More than 80% of the particles are less than 20 microns in size. The presence of sulfide and oxidized minerals of non-ferrous metals requires a special chemical treatment that is associated with the oxidation of sulfides associated with gold [5,10].

The composition of ores is shown in Figure 2.

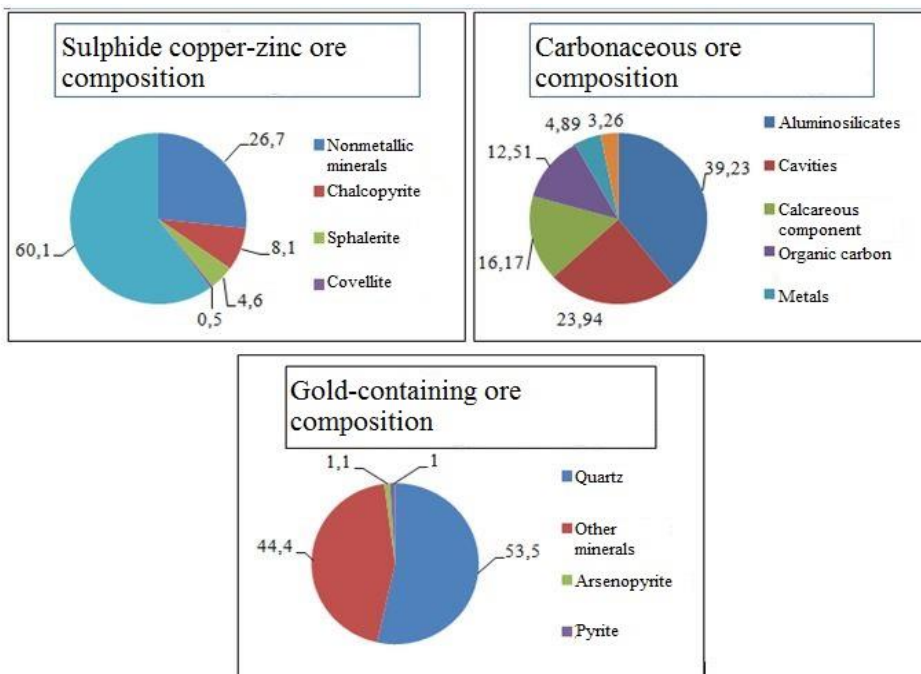


Fig. 2. Mineralogical composition of the ores selected for experiments.

To determine the kinetic dependences of flotation of selected ores, flotation enrichment of the selected raw materials was carried out on a flotation machine JK Flotation Test Batch Machine with subsequent X-ray fluorescence analysis of concentrates on a spectrometer EDX-7000 Shimadzu.

The scheme of experiments is shown in Figure 3.

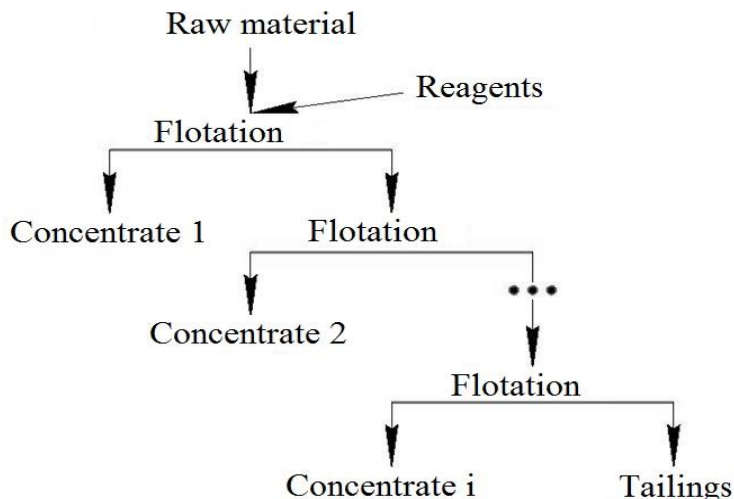


Fig. 3.The scheme of experiments.

The HSC Chemistry 9.0 program was used to evaluate the chemical reaction on the mineral surface through the formation of various products of this reaction. It is an environment for creating models for various types of basic operations from chemical processes to economic optimization. To achieve the set goals of the study, the capabilities of the program to create Pourbaix diagrams were used.

3 Results and discussion

According to the analysis of the obtained data, it is difficult to conclude about the functional form of kinetic dependencies (Table 1). To determine the type of a flotation model, computer programs developed at the Department of Enrichment of Mining University were used. The criterion for selecting suitable dependencies was the coefficient of determination – R^2 .

Table 1. Results of the study of kinetic dependencies.

| Copper-zinc | | Gold-containing | | | | Carbonaceous | |
|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|
| | | Pyrite | | Arsenopyrite | | | |
| Flotation time, s | Total extraction, % | Flotation time, s | Total extraction, % | Flotation time, s | Total extraction, % | Flotation time, s | Total extraction, % |
| 0.00 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30.00 | 12.28 | 30.00 | 4.63 | 30.00 | 1.24 | 60.00 | 12.50 |
| 60.00 | 16.89 | 60.00 | 11.61 | 60.00 | 3.52 | 180.00 | 28.30 |
| 120.00 | 34.96 | 120.00 | 15.56 | 120.00 | 4.94 | 420.00 | 42.30 |
| 240.00 | 53.71 | 240.00 | 19.07 | 240.00 | 5.87 | 720.00 | 54.60 |
| 360.00 | 60.60 | 360.00 | 22.21 | 360.00 | 6.41 | 1800.00 | 68.70 |
| 720.00 | 68.51 | 720.00 | 24.83 | 720.00 | 6.87 | | |

While using an integral method for determining the kinetic dependence of flotation enrichment of copper-zinc ore and gold-containing ore (arsenopyrite flotation), it was found that the Beloglazov equation has a maximum convergence coefficient (Table 2).

Table 2. Results obtained using the integral method.

| Equation | Coefficient | Type of ore | | | |
|---------------------|--------------|-------------|-----------------|--------------|--------------|
| | | Copper-zinc | Gold-containing | | Carbonaceous |
| | | | Pyrite | Arsenopyrite | |
| Beloglazov Equation | R | 0.99814 | 0.99056 | 0.99201 | 0.99625 |
| | R_{∞} | 0.70106 | 0.24831 | 0.06867 | 0.68700 |
| | k | 0.33927 | 0.46820 | 0.58946 | 0.14794 |
| Order 0,5 | R | 0.93669 | 0.91818 | 0.88186 | 0.94661 |
| | φ | 0.16678 | 0.08952 | 0.04556 | 0.09862 |
| | b | 0.30939 | 0.22318 | 0.12674 | 0.33030 |
| Order 1 | R | 0.97284 | 0.97554 | 0.95652 | 0.98933 |
| | φ | 0.45505 | 0.36080 | 0.32905 | 0.40371 |
| | b | -1.41880 | -2.21900 | -3.39840 | -1.70200 |
| Order 1,5 | R | 0.98762 | 0.99007 | 0.97859 | 0.99853 |
| | φ | 1.28100 | 1.54590 | 2.56760 | 1.74430 |
| | b | 0.80141 | 1.52510 | 2.95300 | 0.87740 |
| Order 2 | R | 0.99490 | 0.99494 | 0.98993 | 0.99929 |
| | φ | 3.50840 | 6.17220 | 18.35370 | 7.36340 |
| | b | 1.11490 | 3.51580 | 12.61250 | 1.22020 |

When determining the kinetic dependence using the integral method for flotation of pyrite from sulfide ore and carbon-containing raw materials, it was found that the second-order equation has the maximum convergence (see Table 2). An example of calculation for carbon-containing raw materials is shown in Figure 4.

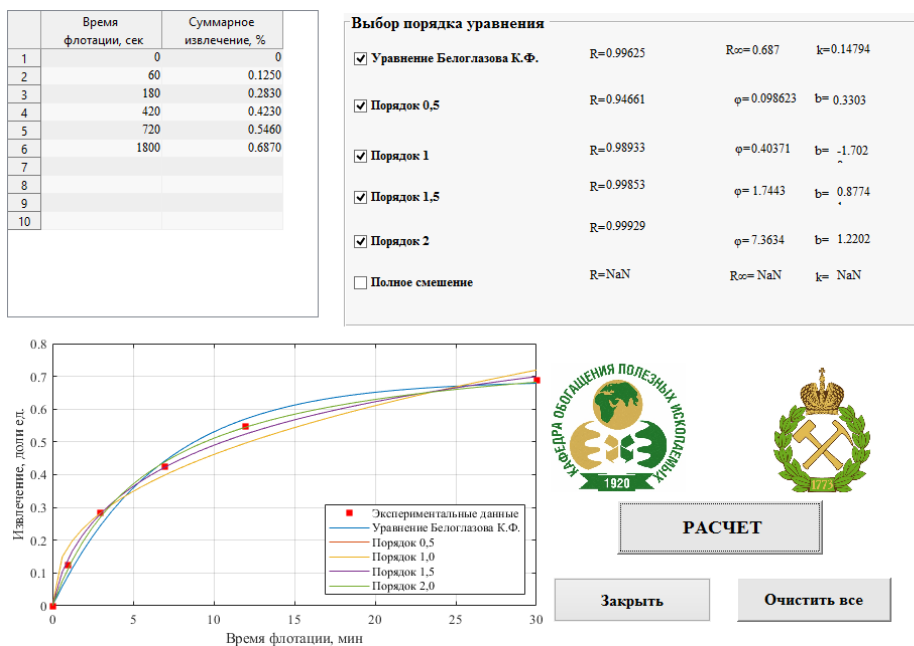


Fig.4. The example of using the program for calculating the kinetic dependence of the integral method for carbon-containing raw materials.

Using the program to determine the constants of the most commonly used equations for copper-zinc ore showed the maximum coefficient of determination for the classical (Beloglazov) model, the Modified Kelsall model, and the Gamma model. Using the program to determine the constants of the most commonly used equations for carbonaceous ore showed that the modified Kelsall model has the maximum convergence with experimental data (Table 3).

Table 3. Results obtained in the analysis of equations.

| Equation | Coefficient | Type of ore | | | Carbonaceous |
|---------------------------|--------------|-------------|-----------------|--------------|--------------|
| | | Copper-zinc | Gold-containing | | |
| | | | Pyrite | Arsenopyrite | |
| Beloglazov Equation | R | 0.99814 | 0.99056 | 0.99211 | 0.996292 |
| | R_{∞} | 0.70106 | 0.24831 | 0.06867 | 0.679 |
| | k | 0.33927 | 0.4682 | 0.058992 | 0.153487 |
| Klimpel Equation | R | 0.99566 | 0.98992 | 0.98787 | 0.996834 |
| | R_{∞} | 0.80643 | 0.26337 | 0.074034 | 0.745606 |
| | k | 0.6309 | 1.0617 | 1.2606 | 0.321071 |
| Kelsall Equation | R | 0.99607 | 0.99545 | 0.99374 | 0.995899 |
| | φ | 0.49757 | 0.81389 | 0.093864 | 0.679795 |
| | k_f | 0.5 | 0.74771 | 0.70902 | 0.5 |
| | k_s | 0.042306 | 0.0067261 | 0.0063787 | 0.027224 |
| Modified Kelsall equation | R | 0.99614 | 0.99556 | 0.99374 | 0.999867 |
| | R_{∞} | 0.70106 | 0.27823 | 0.38567 | 0.701533 |
| | k_f | 0.5 | 0.85305 | 0.70918 | 1.034673 |
| | k_s | 0.33927 | 0.11771 | 0.0018654 | 0.109951 |
| | φ | 1 | 0.43401 | 0.84097 | 0.830996 |
| Gamma model | R | 0.99614 | 0.99496 | 0.99305 | 0.999354 |
| | R_{∞} | 0.70111 | 0.27447 | 0.06867 | 1 |
| | λ | 9596.1085 | 2.1164 | 7.2799 | 2.983695 |
| | P | 3255.6165 | 1.2121 | 4.7946 | 0.476937 |
| Fully mixed model | R | 0.95534 | 0.98556 | 0.98673 | 0.911197 |
| | R_{∞} | 0.6851 | 0.24831 | 0.072536 | 0.679 |
| | k | 1 | 1 | 1 | 1 |

An example of calculation for copper-zinc ore is shown in Figure 5.

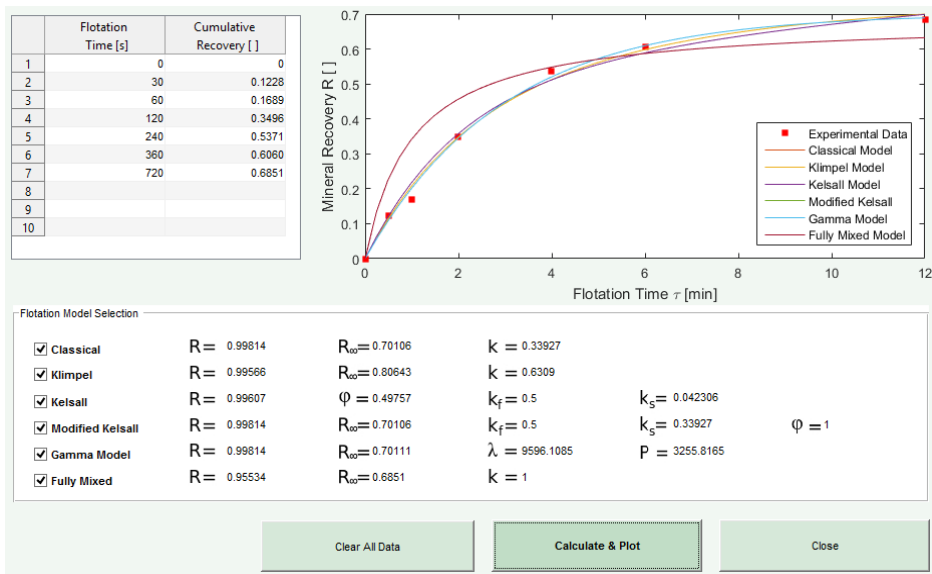


Fig. 5. Using the program to select the most appropriate equation for copper-zinc ore.

When using the program to determine the constants of the most commonly used equations for gold-containing ore, it was found that the Kelsall equation has maximum convergence with the empirical dependence for both pyrite and arsenopyrite flotation (see Table 3).

Analysis of the hydrophobizing ability of the primary collector for the flotation of sulfide of potassium butyl xanthate was carried out in two stages: the wetting angle at the mineral-water-air boundary was determined without treating the mineral surface with a reagent and with its pretreatment by a collector, then the floatability parameter was calculated for both cases (Fig. 6).

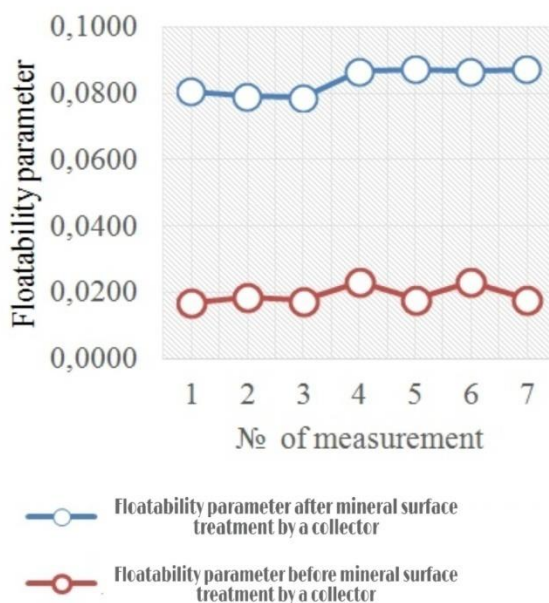


Fig. 6. Floatability parameter before and after mineral surface treatment by the collector.

The floatability parameter F can be calculated using the formula:

$$F = \sigma_{g-l}(1 - \cos\theta) \tag{1}$$

σ_{g-l} is the surface tension at the gas-liquid interface; $\cos\theta$ is the cosine of the wetting angle of the three-phase contact perimeter [4].

Based on the data obtained, it can be concluded that the pyrite surface is hydrophobized, as the obtained values of the wetting angle are higher than 90° , the floatability parameter is increased.

The formation of sulfate ions will be a factor of optimal use of oxidizers in the flotation process. For stable oxidation of the surface of minerals, it is necessary to select the appropriate range of Eh and pH.

The zone of the existence of sulfate ions is characterized by the highest probability of oxidation of the pyrite surface in gold-containing ore [11,12].

When comparing the results of flotation simulation with the use of an oxidizer and without it, an increase in the zone of the existence of sulfate ions is observed by 7.16% (from 1.72 to 1.85) (Fig. 7).

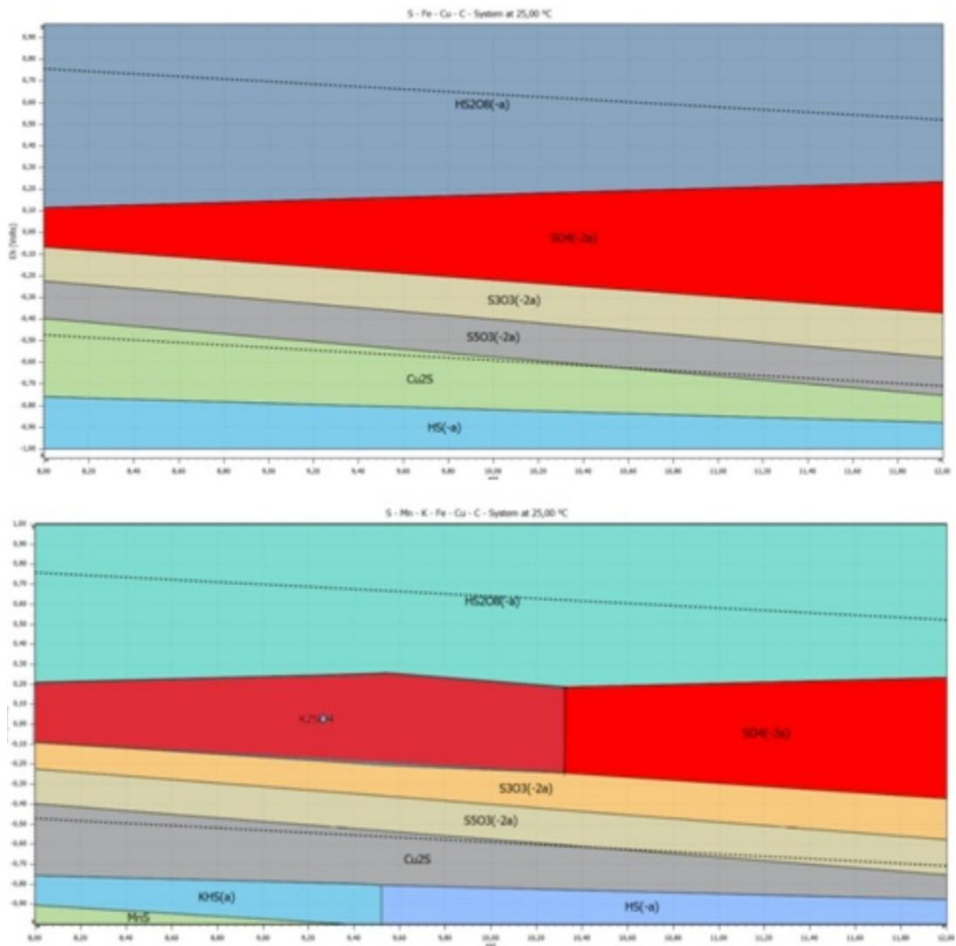


Fig. 7. Model of the flotation process: top-without the use of an oxidizer; bottom-with the use of an oxidizer.

Based on the obtained data, we can conclude about the influence of preliminary mechanical activation of copper-zinc sulfide ores on the technological indicators of their flotation enrichment (Fig. 8).

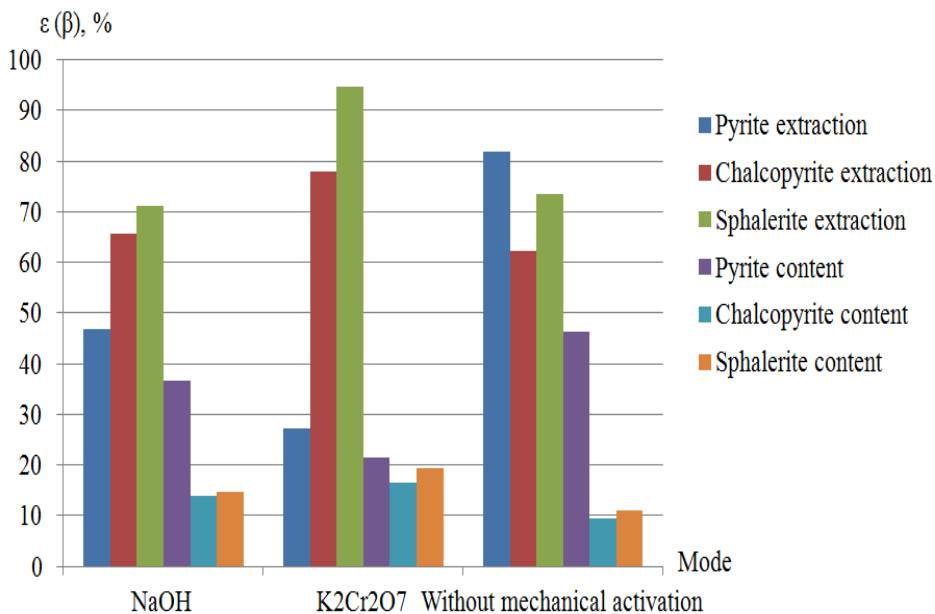


Fig. 8. Estimation of the effect of preliminary mechanical activation of copper-zinc ores.

When adding potassium bichromate as a dispersant, the content of chalcopyrite and sphalerite in the collective concentrate is maximum, which is a positive factor in flotation enrichment. At the same time, the extraction of pyrite is minimal, which can be used at the stage of selective flotation, since the extraction of pyrite in selective copper-zinc concentrates is undesirable since during their further pyrometallurgical processing, a large amount of sulfur contained in iron sulfides is released [13].

4 Conclusion

According to the data obtained in the study of kinetic dependencies of various raw materials, the best convergence results are shown by the Beloglazov equation, the Kelsall model, and the modified Kelsall model.

Technological indicators of sulfide flotation in the presence of oxidants are higher, which can be explained by the intense oxidation of the transition ions formed on the surface of minerals, which helps to align the flotation properties of the surface.

It is possible to integrate the proposed research methods into technological schemes to optimize technological indicators and increase profits.

The work was supported by the Russian Science Foundation (project No. 19-17-00096). We want to express our gratitude to Prof. Tatyana N. Aleksandrova, Dr. of Engineering, Head of the Mineral Processing Department of Mining University.

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