# The effect of seismic base isolation on structural response of a 12story hotel building in Padang, Indonesia

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**Abstract.** The amount of potential investment in Padang City, Indonesia since 2017 attracted many investors to contribute to the city. One of the investments is a 12-story hotel that will be constructed in By Pass Street of the city. The hotel is located in a high seismic zone area, so the seismic base isolation has been proposed to be used in the hotel building. The main aim of using a seismic base isolation device is to reduce the inertia forces introduced in the structure due to earthquakes by shifting the fundamental period of the structure out of dangerous resonance range and concentration of the deformation demand at the isolation system. An analytical study on the Reinforced Concrete (RC) hotel building with and without rubber bearing (RB) base isolation is carried out using the response spectrum and time history analysis methods. The results show that internal forces and inter-story drift of the building with high damping rubber bearing (HDRB) are lower than that of the fixed base with a remarkable margin. From this study, it is recommended to use the HDRB base isolation for medium and high rise buildings with soft soil in Padang City, Indonesia.

# **1** Introduction

The big amount of potential investment in Padang City, the capital city of West Sumatra, made the city win an investment-worthy city award in the Indonesia Attractiveness Award in 2017. As a consequence of the high tourism possibility and hotel occupancy rates in Padang City, an increase of 11.44 points from 52.36% in February 2016 to 64.04% in March 2017, caused a lot of new hotels were constructed in Padang City in last two years.

One of the oncoming hotels is Melia International (MI) hotel that was planned to build a five-star hotel located at km. 16 of by-pass road area, targeted tourists and cross-province road users. Following the limited land, Melia International Hotel will be built vertically with 12 floors with a semi-basement for parking area, the 10<sup>th</sup> floor for hotel functions and the roof floor as a helipad base. However, the construction of the hotel will not be easy because the area is susceptible to earthquake disasters. Also, the land of this area is categorized as soft soil (SE) which has the potential for magnification of earthquake waves [1, 2].

This is not tolerable for buildings whose contents are more costly and valuable than the buildings themselves. Therefore, a special technique to minimize the risks, the base isolation technique is increasingly being adopted. Base isolation is to prevent the superstructure of the building from absorbing the earthquake energy [3, 4]. A structure with base isolator has been supported by isolation elements (such as rubber bearings or sliders), which are typically installed between the building structure and its foundation [5]. During an earthquake, the fixed base structure without seismic isolation is subjected to substantial story drifts, which may lead to damage or even collapse of the building [6, 7].

Therefore, this study, the Moment Resisting Frames with Shear Wall (Dual System) structural system building has been modeled and analyzed for the hotel building using the current earthquake standard code (SNI 1726:2012) and the 2017 earthquake hazard map [8]. The analysis results in terms of structural elements internal forces, story displacement, and inter-story drift were obtained from spectrum response and time history analysis for both fixed base and base-isolated buildings. Finally, it was of interest to check the difference between the responses of a fixed-base building frame and the isolated-base building frame under seismic loading.

# 2. Design and analysis of the building

# 2.1 Preliminary design

The design of structures as thought courses tends to consist of guessing the size of members required in a given structure and analyzing them. The structural members should be designed for optimum use of its materials i.e. steel and concrete [9]. Similarly, at a global level of the structure, the design should be such that, each member should be used optimally. Initial dimensions (preliminary design) of the structural element were detailed by following the steps and standards in SNI 2847:2013 [10].

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#### 2.1.1 The beam

The dimensions of the beam elements were designed according to the SNI 2847:2013, as shown in Table 1.

### 2.1.2 The slab

The dimensions of the building slabs were designed to be 120 mm for the interior floor, 100 cm for concrete floor deck, and 250 mm for the helipad.

Primary Beam		Secondary Beam		
Span (m) h x b <sub>w</sub> (mm)		Span (m)	h x b <sub>w</sub> (mm)	
8	580 x 300	8	540 x 270	
7	560 x 280	7	480 x 260	
6	550 x 280	6	400 x 260	
5.5	550 x 280	5.5	400 x 260	
5	400 x 260	5	380 x 250	
4.8	400 x 260			
4	380 x 250			

**Table 1.** The cross-sectional dimensions of the beams.

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	Interior Column (Primary Building)		Exteri (Seconda	or Column ary Building
Floor	Height (m)	Dimension (mm)	Height (m)	Dimension (mm)
Base- ment	4.5	1400 x 1400	4.5	500 x 500
1 <sup>st</sup>	4.5	1400 x 1400	4.5	500 x 500
2 <sup>nd</sup>	4.5	1400 x 1400	4.5	500 x 500
3 <sup>rd</sup>	4.5	1400 x 1400	4.5	500 x 500
4 <sup>th</sup>	4.15	1200 x 1200	Height '	Total = 18 m
5 <sup>th</sup>	4.15	1200 x 1200		
6 <sup>th</sup>	4	1000 x 1000		
7 <sup>th</sup>	4	1000 x 1000		
8 <sup>th</sup>	4	900 x 900		
9 <sup>th</sup>	4	900 x 900		
10 <sup>th</sup>	3.4	900 x 900		
11 <sup>st</sup>	3.4	900 x 900	]	
Не	eight Total	= 49.1 m		

# 2.1.3 The column

Dimensions of columns were designed based on the SNI 2847:2013 requirements used for the buildings, as given in Table 2.

# 2.1.4 The structural wall

The dimensions of the building shear wall were designed with a thickness of 350 mm and the retaining wall with a thickness of 400 mm.

### 2.2 Modeling of the building structure

In this research, two structural models of a 12-storied fixed base and base-isolated hotel buildings have been modeled and analyzed using structural analysis and design software package ETABS v.16. The fixed base building has been modeled with a fixed support at the base and the base-isolated building has been modeled incorporating rubber bearings near the base of the columns, as shown in Figs. 1 and 2, respectively. Those models included structural components such as RC columns, beams, shear walls for lift cores and slab. Other structural components were an overhead water tank and a helipad.



Fig. 1. The structural modeling of the building without the base isolator.



Fig. 2. The structural modeling of the building with the base isolator.

There is separation on several parts of the baseisolated structure model building to obtain efficiency in the use of base isolators and to meet the requirements of SNI 1726-2012 article 12.2.5.2 [4]. All the procedures for preparing and applying base isolators can be seen in SNI 1726:2012 article 12. Some rules for modeling of base isolators can be explained in the following points.

#### 2.2.1 The examination room

According to SNI 1726:2012 article 12.2.48, the base isolator must have its examination room to facilitate the maintenance and replacement of components in the occurrence of damage. In this building, an examination room is planned with a height of 2 m below the basement. The location of examination rooms and base isolators are shown in Fig. 3.



Fig. 3. The base isolator and its examination room modeling.

#### 2.2.2 The dimension of the base isolator

A base-isolated structure is supported by a series of bearing pads which are placed between the building and the building's foundation. The base isolation system that was used in this building is the high damping rubber bearing (HDRB) with the classification MVBR-0430 (X0.6R). The specifications and characteristics of the base isolator are shown in Tables 3 and 4, respectively.

#### 2.3 Loads

Loads are a primary consideration in any building design, which defines the nature and magnitude of hazards or external forces that a building must resist providing reasonable performance (i.e., safety and serviceability) throughout the structure's useful life [11].

#### 2.3.1 Dead load (D)

Dead loads consist of the permanent construction material loads comprising the roof, floor, wall, and foundation systems, including claddings, finishes, and fixed equipment. The values for dead loads in Table 5 are for commonly used materials and constructions in residential buildings [12].

Table 3. The specification of HDRB.

Properties		Unit	HH 060 x 6R	HH 070 x 6R	HH 080 x 6R
Effective outer diameter	Do	mm	600	700	800
Shear modulus	G	N/mm <sup>2</sup>	0.62	0.62	0.62
Thickness of rubber layer	tr	mm	4	4.7	5.4
Number of rubber layer	n		50	43	37
Total rubber thickness	Tr	mm	200	200	200
First shape factor	S1		36.6	36.4	36.1
Second shape factor	S2		3	3.46	4
Inner of lead diameter	di	mm	15	15	20
Height	Н	mm	407.9	388.3	422.2
Weight	W	kN	6.5	7.9	11.9
Mass		ton	0.66	0.8	1.21

Table 4. The design characteristic of HDRB.

Propertie	s	Unit	HH 060 x 6R	HH 070 x 6R	HH 080 x 6R
Normal stress	$\sigma_{s}$	N/mm <sup>2</sup>	6.6	9.1	12
Shear stiffness	Kh	.10 <sup>3</sup> kN /m	0.876	1.18	1.56
Initial shear stiffness		.10 <sup>3</sup> kN /m	5.19	6.99	9.23
Eff Damping Ratio			0.24	0.24	0.24
Ult. comp. stress	$\sigma_{c}$	N/mm <sup>2</sup>	7.4	1.6	4.11
Ult. tensile stress	$\sigma_{tu}$	N/m <sup>2</sup>	1	1	1
Compressive stiffness	Kv	.10 <sup>3</sup> kN /m	1970	2660	3510
Strength of yield	KN		71.5	97.3	127
Ult. displacement	d/2	mm	300	350	400

# 2.3.2 Earthquake load (E)

Earthquake forces experienced by a building result from ground motions (accelerations) which are also fluctuating or dynamic they reverse direction somewhat chaotically [13]. Earthquake load is assumed as a vibration that gives cyclic load on buildings horizontally and vertically. As for this design, the earthquake acceleration in Padang was taken from the 2017 earthquake map with the parameters of the earthquake spectral response shown in Table 6.

Table 5. Additional dead load.

No.	Type of load	Weight	Unit
1	Steel	78,5	kN/m <sup>3</sup>
2	Concrete	22	kN/m <sup>3</sup>
3	River Stone	22	kN/m <sup>3</sup>
4	Mortar	22	kN/m <sup>3</sup>
5	Reinforced Concrete	24	kN/m <sup>3</sup>
6	Sand	16	kN/m <sup>3</sup>
7	Asphalt Coating	14	kN/m <sup>2</sup>
8	Water	10	kN/m <sup>2</sup>
9	Stonemasonry wall 1/2 pair	2,5	kN/m <sup>2</sup>
10	Curtain Wall + frame	0,6	kN/m <sup>2</sup>
11	Ceiling and hanger	0,2	kN/m <sup>2</sup>
12	Cladding metal sheet + frame	0,2	kN/m <sup>2</sup>
13	Floor Finishing	22	kN/m <sup>3</sup>
14	Marble, granite per cm thick	0,24	kN/m <sup>2</sup>
15	Plumbing installation (ME)	0,25	kN/m <sup>2</sup>
16	Tile roof coverings	0,5	kN/m <sup>2</sup>

From these data, the earthquake load can be simulated using spectrum response analysis and time history. Here, equivalent static analysis cannot be used because it does not meet the requirements of SNI 1726-2012 article 7.7.2. The analysis of time history is used because of the use of base isolators for SE site class.

• Response spectrum analysis

The response spectrum represents an envelope of upper bound responses, based on several different ground motion records. This method is an elastic dynamic analysis approach that relies on the assumption that dynamic response of the structure may be found by considering the independent response of each natural mode of vibration and then combining the response of each in the same way [14]. The spectrum dynamic response seismic loads based on SNI 1726:2012 are used in dynamic response analysis by adjusting the site classification and seismicity level in Padang City, as shown in Fig. 4.

• Time history analysis

Seismic loads are also generated in a structure by imposing ground accelerations. Dynamic time history analysis has been carried out on two buildings. Analysis procedures are available to compute the response of a structure to this type of load. In this study, the time versus ground acceleration graph of the Padang City earthquake, 2009 shown in Figs. 5 and 6, was used for the time history analysis.



Fig. 4. The acceleration response spectrum of Padang City for soft soil.

Table 6. The earthquake load parameters.

Parameter (SNI 1726:2012)	Varia ble	Value	Info/ Unit
Risk category		III	
Importance factor	Ie	1	
	Ss	1.5	g
The spectral response acceleration values	$\mathbf{S}_1$	0.6	g
	PGA	0.6	g
Soil site class	N SPT	7.71	SE
(Standard Penetration Test value N, and shear wave velocity V <sub>s</sub> )	Vs	240; 227; 242	SD
	Fa	1.35	g
Seismic amplification factors	$\mathbf{F}_{\mathbf{v}}$	1.44	g
	Fpga	0.54	g
The spectral response	$\mathbf{S}_{\mathrm{MS}}$	1.35	g
acceleration parameters corresponding to the soil site	$S_{M1}$	1.44	g
class	$PGA_m$	0.54	g
The value of the design	S <sub>DS</sub>	0.90	g
at short periods and at a 1- second period	$S_{D1}$	0.96	g
Seismic design category	KDS	D	
	T <sub>0</sub>	0.21	sec
	Ts	1.07	sec
	$C_u$	1.40	
Fundamental period	$\mathbf{C}_{t}$	0.0466	
	Х	0.90	
	hn	44.10	m
	Ta	1.41	sec
Seismic Response Factor,	R	7	
reduction factor of the building	Ω	2.5	
structure (Dual system, shear wall with SRMF)	$C_d$	5.5	

• Wind load (W)

For buildings that have a height of more than 9 meters, the wind load should be simulated on the building. As for the International Melia Hotel with a height of 44.1 meters, wind load analysis was carried out using the Main Wind Load Retaining System with the following wind load parameter data:

a) Building risk categories	= III
b) Basic Wind Speed of Padang	= 26  km/h
c) Wind Direction Factor, K <sub>d</sub>	= 0.85
d) Surface Roughness	= C
e) Exposure Category	= C
f) Topographic Factors, K <sub>zt</sub>	= 1
g) Classification of closure	= semi
h) Internal pressure coefficient, G <sub>Cpi</sub>	= 0.55
i) Wind effect factors	= 0.85
j) Exposure coefficient of velocity	= 1.37
pressure k <sub>h</sub> and k <sub>z</sub>	
k) Velocity pressure, $q_z$	=37.2 N/m <sup>2</sup>



**Fig. 5.** Ground motion data for Padang Earthquake in 2009 (direction: north-south).



**Fig. 6.** Ground motion data for Padang Earthquake in 2009 (direction: east-west).

# 3. Analysis results

#### 3.1 Internal forces comparison

This study demonstrated that the response was mainly affected by the incorporation of rubber bearings used as base isolators. To carry out a comparison between fixed base and base-isolated building by dynamic method on the bases of response properties like internal forces (axial, shear, and bending moment) in structural elements (beam and column), the point of view of internal force element is determined based on Fig. 7.



Fig. 7. The structural elements point of view.

#### 3.1.1 Interior beam

The internal forces comparison on the fixed base and base-isolated buildings of the interior beam are shown in Tables 7 and 8. Though while comparing the base of the structure, the base-isolated structure has the least value of internal forces and the percentage reduction is 14.09% and 24.76% for shear force and bending moment, respectively. However, there is an increase of internal forces in the ground floor due to the use of the base isolators. It is indicated that the structure on the ground floor must be more stiffness in the structural design.

 Table 7. The comparison of beam shear forces for the fixed base and base-isolated buildings.

Stowy	Elev.	Span	Shear Force (kg)		Shear Force (kg)		Reducti
Story	(m)	(m)	Fixed	Base Isolator	on (%)		
Helypad	44.1	6	4560	4684	-2.71		
11	40.7	6	3754	3761	-0.19		
10	37.3	6	2939	2082	29.17		
9	33.3	6	2988	2115	29.22		
8	29.3	6	3043	2180	28.38		
7	25.3	6	2984	2173	27.17		
6	21.3	6	3026	2263	25.23		
5	17.2	6	2864	2215	22.66		
4	13.1	6	2638	2175	17.56		
3	9	6	2329	2071	11.05		
2	4.5	6	3905	3911	-0.16		
1	0	6	3924	3926	-0.05		
Basement	-4.5	6	3226	3357	-4.06		

Story	Elev.	Span	Ber Mome	nding nt (kgm)	Reducti
Story	(m)	(m)	Fixed	Base Isolator	on (%)
Helypad	44.1	6	9107	6107	32.94
11	40.7	6	9249	6068	34.39
10	37.3	6	6256	4035	35.50
9	33.3	6	6371	4116	35.40
8	29.3	6	6434	4241	34.07
7	25.3	6	6242	4232	32.19
6	21.3	6	6186	4413	28.66
5	17.2	6	5749	4328	24.71
4	13.1	6	5142	4255	17.24
3	9	6	4434	4063	8.37
2	4.5	6	4946	5496	-11.11
1	0	6	3086	4921	-59.42
Basement	-4.5	6	1671	4220	-152.44

Table 8. The comparison of beam bending moment for th	e
fixed base and base-isolated buildings.	

### 3.1.2 Interior column

The internal forces comparison on the fixed base and base-isolated buildings of the interior column are shown in Tables 9, 10, and 11.

 Table 9. The comparison of column axial force for the fixed base and base-isolated buildings.

Stowy	Elev.	Heig Axial F		orce (kg)	Reducti
Story	(m)	(m)	Fixed	Base Isolator	on (%)
Helypad	44.1	3.4	2862	1745	39.04
Roof	43.7	3	7512	4612	38.60
11	40.7	3.4	16457	5202	68.39
10	37.3	4	55774	6517	88.32
9	33.3	4	116359	11156	90.41
8	29.3	4	203462	32240	84.15
7	25.3	4	298527	62913	78.93
6	21.3	4.1	465455	112506	75.83
5	17.2	4.1	622754	168277	72.98
4	13.1	4.1	840695	249413	70.33
3	9	4.5	1003013	324674	67.63
2	4.5	4.5	1149690	404947	64.78
1	0	4.5	1234356	485381	60.68
Basement	-4.5	2	1232161	559221	54.61

Stowy	Elev.	Heig	Shear Fo	Reducti		
Story	(m)	m (m)	Fixed	Base Isolator	on (%)	
Helypad	44.1	3.4	4141	2569	37.94	
Roof	43.7	3	4272	1901	55.49	
11	40.7	3.4	2650	657	75.18	
10	37.3	4	5801	1403	75.81	
9	33.3	4	7499	1754	76.60	
8	29.3	4	10255	2400	76.59	
7	25.3	4	12475	2719	78.20	
6	21.3	4.1	19046	4138	78.27	
5	17.2	4.1	22116	5037	77.22	
4	13.1	4.1	32351	7898	75.58	
3	9	4.5	33394	8470	74.64	
2	4.5	4.5	43014	9664	77.53	
1	0	4.5	23703	10703	54.84	
Basement	-4.5	2	49426	11714	76.30	

 Table 10. The comparison of column shear forces for the fixed base and base-isolated buildings.

 Table 11. The comparison of column bending moment for the fixed base and base-isolated buildings.

Stowy	Elev.	Heig	Bending (kg	Reducti		
Story	(m)	m (m)	Fixed	Base Isolator	on (%)	
Helypad	44.1	3.4	2536	2603	-2.66	
Roof	43.7	3	4351	2779	36.13	
11	40.7	3.4	2295	851	62.88	
10	37.3	4	5090	2066	59.41	
9	33.3	4	7584	2139	71.79	
8	29.3	4	12282	2667	78.28	
7	25.3	4	16390	3044	81.42	
6	21.3	4.1	28856	5573	80.69	
5	17.2	4.1	37082	7380	80.10	
4	13.1	4.1	54938	11399	79.25	
3	9	4.5	68746	14901	78.32	
2	4.5	4.5	97556	17737	81.82	
1	0	4.5	75756	21316	71.86	
Basement	-4.5	2	51255	14466	71.78	

When comparing the fixed base and base-isolated structures, the percentage reductions of internal forces for base-isolated structures are 68.19%, 70.72%, and 71.82% for axial, shear forces, and bending moment, respectively. But on the helipad floor, there is an increase in bending moment. It is indicated by the large stiffness in the short column of the helipad.

#### 3.2 The comparison of displacement and interstory drift



**Fig. 8.** The comparison of displacement for the fixed base and base-isolated buildings in the X direction.



**Fig. 9.** The comparison of displacement for the fixed base and base-isolated buildings in the Y direction.

Story	Elev.	Displacement (mm)		Inter-story Drift (mm)		Reduct
	(m)	Fixed	Isolat or	Fixed	Isolat or	10n (%)
Helypad	44.1	58.9	160.5	0.6	0.28	52.18
Roof	43.7	58.3	160.2	4.6	2.18	52.64
11	40.7	53.7	158.0	5.3	2.51	52.86
10	37.3	48.4	155.5	6.1	2.98	51.43
9	33.3	42.2	152.6	5.9	3.00	49.41
8	29.3	36.3	149.6	5.9	3.01	49.28
7	25.3	30.4	146.5	5.7	3.00	47.90
6	21.3	24.6	143.5	5.6	3.02	46.16
5	17.2	19.0	140.5	5.2	2.94	43.75
4	13.1	13.8	137.6	4.4	2.82	36.49
3	9	9.4	134.8	3.7	2.17	40.72
Pool deck	5.7	5.7	132.6	1.0	0.75	24.30
2	4.5	4.7	131.8	2.9	2.67	9.97
1	0	1.7	129.2	1.7	2.35	-35.61
Base- ment	-4.5	0.0	126.8	0.0	0.92	-100.0
Mainte- nance	-6.5	0.0	125.9			

Table 12. The comparison of inter-story drift for the fixed base	
and base-isolated buildings in the X direction.	

Story	Elev.	Displacement (mm)		Inter-story Drift (mm)		Reduct
	(m)	Fixed	Isolat or	Fixed	Isolat or	(%)
Helypad	44.1	80.1	160.8	-2.46	-25.04	-916.7
Roof	43.7	82.5	185.8	6.14	2.89	52.96
11	40.7	76.4	182.9	7.07	3.31	53.11
10	37.3	69.3	179.6	8.49	3.94	53.66
9	33.3	60.8	175.5	8.67	3.98	54.04
8	29.3	52.2	171.7	8.67	3.91	54.90
7	25.3	43.5	167.8	8.50	3.69	56.53
6	21.3	34.9	164.1	8.20	3.75	54.27
5	17.2	26.8	160.4	7.25	3.44	52.54
4	13.1	19.5	156.9	6.52	3.21	50.77
3	9	13.0	153.7	4.63	2.50	46.06
Pool deck	5.7	8.4	151.2	1.17	0.88	25.06
2	4.5	7.2	150.3	4.80	3.14	34.54
1	0	2.4	147.2	2.42	2.79	-15.64
Base- ment	-4.5	0.0	144.4	0.00	1.11	-100.0
Mainte- nance	-6.5	0.0	143.3			

Story displacements are plotted graphically in Figs. 8 and 9. Displacement of the structure building subjected to time history analysis is recorded in each node in both X and Y directions. There is no displacement is recorded at the base since the base is in the fixed condition. The reduction of inter-story drift between fixed base and base isolator building for X and Y directions are shown in Tables 12 and 13, respectively. The use of HDRB base isolator reduces the inter-story drift by around 56.53%, but, there is an increase in deviation on the helipad since the large stiffness in their short columns.

# 4. Conclusions

Dynamic Response Spectrum and Time History Analysis are carried out for the Melia International Hotel building. The building is modeled and analyzed using fixed base and base-isolated structures. The comparison of structure responses between fixed and base-isolated building structures like internal forces in structural elements, story displacement, and inter-story drift has been done. The results of the analysis can be summarized as follow:

1. The maximum reduction in beam's internal forces of shear force and bending moment is 29.22% and 35.50%, respectively when isolated with HDRB as compared to the fixed base condition. Also, the column's internal forces of base-isolated structures reduced by average 68.19% for axial, 70.72% for shear, and 71.82% for bending moment compared to the fixed base structure.

Table 13. The comparison of inter-story drift for the fixed base	
and base-isolated buildings in the Y direction.	

- 2. On the ground floor, there is an increase in the beam's internal forces due to the use of the base isolators. It is indicated that the structure of the ground floor must be given more stiffness. Also, on the helipad floor, there is an increase in the column's internal force due to the large stiffness in the short column of the helipad.
- 3. There is no displacement recorded at the base since the base is in the fixed condition. There is a 56.53% reduction in an inter-story drift on the base-isolated structure compared to the fixed-base structure.
- 4. From this study, it was proved that the performance of the base-isolated building is much better compared to the fixed base building. So, it is recommended to use the HDRB base isolation for medium and high rise buildings in Padang City, Indonesia, especially in soft soil conditions.

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